

SEMICONDUCTOR INTEGRATED CIRCUIT

BACKGROUND OF THE INVENTION

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Field of the Invention

The present invention relates to a semiconductor integrated circuit, provided with an improved characteristic impedance of the signal transmission line of a semiconductor integrated circuit, capable of reducing 10 coupling with other transmission lines.

Background Art

Conventionally, when providing a signal transmission line with a microstrip structure constituted by a signal line and a ground plate in a 15 semiconductor integrated circuit, two separate wiring layers for the signal line and for the ground plate are used as shown in Fig. 8.

In order to increase the characteristic impedance of this signal transmission line in a signal transmission line of a microstrip structure composed of the integrated signal lines and a ground plate, two methods have 20 been adopted, one method is to make the signal line width narrower, and the other method is to increase the distance d between the signal line and the ground plate.

Furthermore, the other conventional technique is disclosed in Japanese

Unexamined Patent Application, No. Hei 5-343564, which determines the characteristic impedance of the transmission line by a mesh-like mesh ground plane, and the spaces corresponding to the pores of the mesh are compensated for by the ground plate.

5 However, when the above-described first method for making the signal line width narrower is adopted, the problem arises that the maximum input capacitance of a circuit connected to the end of the signal transmission line becomes small.

When the above-described second method of increasing the distance d
10 between the signal line and the ground plane is adopted, the problem is encountered that the thickness or the number of wiring layers increases, because it is necessary to increase the thickness of the interlayer films of the wiring layers or to increase the number of wiring layers.

When the third method disclosed in Japanese Unexamined Patent Application, First Publication No. Hei 5-343564 is adopted, although it is possible to increase the impedance of the signal transmission line, the problem arises that, when assembling into an integrated circuit, since the signal lines cannot be formed under the ground plane, it is not possible to avoid generating coupling between a plurality of signal lines.

20 When coupling occurs, a deficiency arises that in the characteristic impedance of a certain signal line will experience a dynamic change, because the capacitance between one signal line and its counter line changes when the voltage level of the counter signal line changes.

In addition, the problem also arises in the case of using a mesh ground plane that it is difficult to evaluate the characteristic impedance, since the electro-magnetic field generated through small holes or spaces cannot be accurately understood.

SUMMARY OF THE INVENTION

This invention has been made to solve the above-described problems.

It is, therefore, an objective of the present invention to provide a semiconductor device, capable of reducing the coupling between a plurality of 10 signal lines by increasing the characteristic impedance of the signal transmission line of a microstrip structure, which can be realized in a semiconductor device.

According to the first aspect of the present invention, a semiconductor integrated circuit comprises a signal transmission line of a microstrip structure composed of a signal line and a ground plate, wherein at least one 15 hole is formed in said signal line.

According to the second aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate, at least one hole is formed in said ground 20 plate.

According to the third aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate according to the second aspect, the size of said

at least one hole formed in said ground plate is determined such that the AC coupling between the signal line and another signal line disposed close to one signal line and on the opposite side of said ground plate is decreased and the characteristic impedance of said signal transmission line is increased.

5 According to the fourth aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate according to the second aspect, the number of said at least one hole formed in said ground plate is determined such that the AC coupling between one signal line and another signal line disposed close to one signal line and on the opposite side of said ground plate is decreased and the characteristic impedance of said signal transmission line is increased.

10 10 According to the fourth aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate according to the second aspect, the number of said at least one hole formed in said ground plate is determined such that the AC coupling between one signal line and another signal line disposed close to one signal line and on the opposite side of said ground plate is decreased and the characteristic impedance of said signal transmission line is increased.

15 According to the fifth aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate, at least one hole is formed in both of said signal line and said ground plate.

According to the sixth aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate according to the fifth aspect, the size of said at least one hole formed in said ground plate among the signal line and the ground plate is determined such that the AC coupling between one signal line and another signal line disposed close to one signal line and on the opposite side of said ground plate is decreased and the characteristic impedance of said signal transmission line is increased.

20 According to the sixth aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate according to the fifth aspect, the size of said at least one hole formed in said ground plate among the signal line and the ground plate is determined such that the AC coupling between one signal line and another signal line disposed close to one signal line and on the opposite side of said ground plate is decreased and the characteristic impedance of said signal transmission line is increased.

According to the seventh aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate according to the fifth aspect, the number of said at least one hole formed in said ground plate among holes formed in both 5 of the signal line and the ground plate is determined such that the AC coupling between one signal line and another signal line disposed close to one signal line and on the opposite side of said ground plate is decreased and the characteristic impedance of said signal transmission line is increased.

According to the eighth aspect, in a semiconductor integrated circuit 10 comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate according to the second aspect, said at least one hole in said ground plate is formed at a position where the other signal line is not disposed or said at least one hole in said ground plate is made small so as to reduce the AC coupling with one signal line when formed at a 15 position where the other signal line is disposed.

According to the ninth aspect, in a semiconductor integrated circuit comprising a signal transmission line of a microstrip structure composed of a signal line and a ground plate according to the first aspect, where, instead of at least one hole formed in said signal line or in said ground plate, a plurality 20 of slit holes are formed by forming said signal line or said ground plate of a plurality of thin strips and by connecting these thin strips at those terminal ends.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a diagram showing the structure of the signal transmission line according to the first embodiment of the present invention.

Fig. 2 is a diagram showing the structure of the signal transmission line according to the second embodiment of the present invention.

Fig. 3A and Fig. 3B are diagrams showing the relationship between signal lines and a ground plate provided with a single slit.

Fig. 4 is a diagram showing the relationship between signal lines and a ground plate provided with the slit divided into three slits.

Fig. 5 is a graph showing the relationship between the slit width and magnitude of the coupling.

Fig. 6 is a graph showing the slit width in the ground plate and the characteristic impedance.

Fig. 7 is a diagram showing the structure of a signal transmission line according to the third embodiment of the present invention.

Fig. 8 is a diagram showing the structure of a conventional signal transmission line.

DETAILED DESCRIPTION OF THE INVENTION

Hereinafter, the present embodiments of the present invention will be described with reference to the drawings.

<First Embodiment>

Fig. 1 is a diagram showing the structure of the signal transmission line according to the first embodiment of the present invention.

As shown in Fig. 1, in the signal transmission line of the microstrip 5 structure realized in a semiconductor device according to the present embodiment, at least one hole 13 (normally, a plurality of holes 13) is formed on a signal line of a microstrip structure composed of a signal line 11 and a ground plate 12.

In a signal transmission line of the microstrip structure, the 10 characteristic impedance Z is expressed by the equation,

$$Z = (L/C)^{1/2}$$

where C represents the inter-wiring capacitance per unit length, and L represents the inductance of the wiring.

The provision of a hole (or a plurality of holes) in the signal line 11 15 lengthen the electric force line generated between the signal line 11 and the ground plate 12 and the distance between the signal line 11 and the ground plate 12 is apparently elongated equivalently, which results in a decrease of the inter-wiring capacitance C .

When the velocity of the electro-magnetic wave is represented by v , the 20 velocity v is constant and is expressed by the following equation.

$$v = 1/(LC)^{1/2}$$

Thus, when the capacitance C decreases, the wiring inductance L increases.

Consequently, the characteristic impedance can be increased by forming more than one hole in the signal line.

In addition, the increase of the characteristic impedance as shown above makes it possible to suppress the reduction of the maximum input 5 capacitance of the circuit connected at the end of the signal transmission line, and the increase of the characteristic impedance does not require an increase in the number of wiring layers.

The size of the hole 13 in the signal line shown in Fig. 1 can be determined as follows. The size of the hole is determined so as to reduce the 10 wiring resistance as much as possible. At the same time, the size of the hole is determined so as to sufficiently increase the characteristic impedance between the signal line 11 and the ground plate 12 as much as possible.

The number of holes 13 in the signal line 11 may be determined so as to fulfill the following conditions. The number can be decreased to reduce the 15 wiring resistance as much as possible, and the number can be increased to increase the characteristic impedance as much as possible.

It is noted that, instead of forming one signal line as shown in Fig. 1, the signal line may be formed by a plurality of signal line strips spaced apart from each other by slits and the plurality of signal line strips are connected at 20 a certain portion such as both termination ends for forming a plurality of slit-like holes.

<Second Embodiment>

Fig. 2 is a diagram showing the structure of the signal transmission line according to the second embodiment of the present invention.

As shown in Fig. 2, in the signal transmission line of the microstrip 5 structure realized in a semiconductor device according to the second embodiment, at least one hole 24 (normally, a plurality of holes 24) is formed on the ground plate 22 of a microstrip structure composed of a signal line 21 and a ground plate 22.

In the signal transmission line of the microstrip structure, the 10 characteristic impedance Z is expressed by the equation,

$$Z = (L/C)^{1/2}$$

where C represents the inter-wiring capacitance per unit length, and L represents the inductance of the wiring.

The provision of a hole (or a plurality of holes) in the ground plate 22 15 lengthen the electric force line generated between the signal line 11 and the ground plate 12 and the distance between the signal line 11 and the ground plate 12 is apparently elongated equivalently, which results in a decrease of the inter-wiring capacitance C .

When the velocity of an electro-magnetic wave is represented by v , the 20 velocity v is constant and is expressed by the following equation.

$$v = 1/(LC)^{1/2}$$

Thus, when the capacitance C decreases, the wiring inductance L increases.

Consequently, the characteristic impedance can be increased by forming more than one hole in the ground plate 22.

As described above, it becomes possible to suppress the reduction of the maximum input capacitance of the circuit connected at the end of the signal 5 transmission line, and it is not necessary to increase the number of wiring layers.

The size of the hole 24 in the ground plate shown in Fig. 2 can be determined as follows. The size of the hole is determined to reduce the AC coupling between two signal lines 21 adjacent to each other above the hole 24 10 in the ground plate 22 as much as possible. At the same time, the size of the hole is determined to sufficiently increase the characteristic impedance between the signal line 11 and the ground plate 12 as much as possible.

The number of holes 24 in the ground plate shown in Fig. 2 can be determined so as to fulfill the following conditions. The number can be 15 decreased to reduce the AC coupling between two signal lines 21 adjacent to each other above hole 24 in the ground plate 22 as much as possible, and the number of the holes is determined to increase the characteristic impedance between the signal line 21 and the ground plate 22 as much as possible.

20 Next, the magnitude of the coupling and the characteristic impedance are explained based on the results of simulations in the case of forming the ground plate 22 by a plurality of ground plates, separated by slit-like spaces, with reference to Figs. 3 to 6.

Fig. 3A is a cross-sectional view of one transmission line comprising one signal line 21 of $1.2 \mu \text{ m}$ in width and $0.6 \mu \text{ m}$ in thickness, and a ground plate, divided into two plates, each having a width of $50 \mu \text{ m}$, by a single slit of width w , wherein the ground plate is located spaced by a distance d from the signal line. Fig. 3B is a cross-sectional view of a transmission line comprising the signal line shown in Fig. 3A and a ground plate divided into four parts, having a width of $25 \mu \text{ m}$, by three slits, each having a width of $w/3$, and these four parts are separated by three slits each having a width of w , wherein the ground plate is separated from the signal line by a distance of $0.6 \mu \text{ m}$.

Fig. 4 is a schematic diagram showing the capacitance between one signal line 21 and a ground plate 22 having a slit, and the other signal line 23. It is assumed that the capacitance between the signal line 21 and the ground plate 22 is represented by C_g , and the capacitance between the signal line 21 and the other signal line 23 is represented by C_{13} .

Fig. 5 is a diagram showing the relationship between the total slit width and a value of C_{13}/C_g , wherein three lines are shown, in which the dashed line shows the case that the ground plate is divided by a single slit and the distance between the ground plate and the signal line is $0.6 \mu \text{ m}$, the dashed and dotted line shows the case that the ground line is divided by a single slit and the distance between the ground plate and the signal line is $1.8 \mu \text{ m}$, and the solid line shows the case that the ground plate is divided into four parts and the distance between the ground plate and the signal line is $0.6 \mu \text{ m}$. It

is noted that the value of C_{13}/C_g represents the magnitude of the coupling between one signal line 21 with the other signal line 23.

In Fig. 5, when an allowable value of the coupling is assumed to be $C_{13}/C_g = 0.2$, the total slit widths in the respective cases must be restricted to 5 within $3 \mu m$, $4.5 \mu m$, and $9 \mu m$ or less, and the total slit width cannot exceed these values.

<Third Embodiment>

Fig. 7 is a diagram showing the structure of a semiconductor integrated 10 circuit according to the third embodiment of the present invention.

As shown in Fig. 7, in the signal transmission line of the microstrip structure realized in a semiconductor device according to the present embodiment, at least one hole 33 (normally, a plurality of holes 33) is formed on the signal line and the ground plate of the microstrip structure composed 15 of the signal line 31 and the ground plate 32.

In a signal transmission line of the microstrip structure, the characteristic impedance Z is expressed by the equation,

$$Z = (L/C)^{1/2}$$

where, C represents the inter-wiring capacitance at an unit length, and L 20 represents the inductance of the wiring.

The provision of a hole (or a plurality of holes) in both of the signal line 31 and the ground plate 32 lengthen the electric force line generated between the signal line 31 and the ground plate 32 and the distance between the

signal line 31 and the ground plate 32 is apparently elongated equivalently, which results in a decrease of the inter-wiring capacitance C.

When the velocity of an electro-magnetic wave is represented by v, the velocity v is a constant and is expressed by the following equation.

5 $v = 1/(LC)^{1/2}$

Thus, when the capacitance C decreases, the wiring inductance L increases.

Consequently, it becomes possible to suppress the reduction of the maximum input capacitance of the circuit connected at the end of the signal 10 transmission line, and it is not necessary to increase the number of wiring layers.

The size of the hole 33 in the ground plate 32 shown in Fig. 7 can be determined as follows. The size of the hole is determined to reduce the AC coupling between two adjacent signal lines 31 on the hole 33 in the ground 15 plate 32 as much as possible, and the size of the hole is determined to increase the characteristic impedance between the signal line 21 and the ground plate 32 as much as possible.

The number of holes is determined so as to reduce the AC coupling between two signal lines 31 adjacent on the hole 33 in the ground plate 32 as 20 much as possible, and so as to increase the characteristic impedance between the signal line 31 and the ground plate 32 as much as possible.

It is noted that it may be possible, instead of forming holes in the signal line and the ground plate, to constitute the signal transmission line by

forming the signal line and the ground plate by a plurality of strips, and by connecting these strips at, for example, both termination ends of these strips so as to provide a plurality of slit-like holes between each of these strips.

The present invention was described above in detail by explaining the 5 first to the third embodiments. However, the present invention is not limited to these three embodiments described above, but variants thereof can be envisaged without exceeding the scope of the present invention.

For example, the present invention includes the case of both of the signal line and the ground plate having holes together with slits.

10 Furthermore, in the above embodiments, one signal line is disposed on the ground plates. However, the ground plate may be disposed on the signal line, and the ground plate may occupy the most significant position. Such a disposition allows the ground plate to exhibit a shielding effect. In this case, the ground plate may be formed simultaneously with the formation of the 15 bonding pads on the passivation film, which simplifies the manufacturing process.

As described above, in a signal transmission line of a microstrip structure composed of the signal line and the ground plate, the present invention shows a notable effect in that the capacitance between wiring can 20 be decreased and the characteristic impedance between the signal line and the ground plate can be increased by forming holes in the signal line or in the ground plate.

The other effect of the present invention is that the coupling between

one signal line with another signal line through the ground plate can be reduced by forming holes in the ground plate.